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In vivo lung morphometry with hyperpolarized ³He diffusion MRI: Theoretical background

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Abstract

MRI-based study of ³He gas diffusion in lungs may provide important information on lung microstructure. Lung acinar airways can be described in terms of cylinders covered with alveolar sleeve [Haefeli-Bleuer, Weibel, Anat. Rec. 220 (1988) 401]. For relatively short diffusion times (on the order of a few ms) this geometry allows description of the ³He diffusion attenuated MR signal in lungs in terms of two diffusion coefficients—longitudinal (D_L) and transverse (D_T) with respect to the individual acinar airway axis [Yablonskiy et al., PNAS 99 (2002) 3111]. In this paper, empirical relationships between D_L and D_T and the geometrical parameters of airways and alveoli are found by means of computer Monte Carlo simulations. The effects of non-Gaussian signal behavior (dependence of D_L and D_T on *b*-value) are also taken into account. The results obtained are quantitatively valid in the physiologically important range of airway parameters characteristic of healthy lungs and lungs with mild emphysema. In lungs with advanced emphysema, the results provide only "apparent" characteristics but still could potentially be used to evaluate emphysema progression. This creates a basis for *in vivo* lung morphometry—evaluation of the geometrical parameters of acinar airways from hyperpolarized ³He diffusion MRI, despite the airways being too small to be resolved by direct imaging. These results also predict a rather substantial dependence of ³He ADC on the experimentally-controllable diffusion time, Δ . If Δ is decreased from 3 ms to 1 ms, the ADC in normal human lungs may increase by almost 50%. This effect should be taken into account when comparing experimental data obtained with different pulse sequences. © 2007 Elsevier Inc. All rights reserved.

Keywords: Diffusion MRI; Hyperpolarized gas; Lung airways; Apparent diffusion coefficient

1. Introduction

Hyperpolarized ³He gas and some other hyperpolarized gases are now broadly used in MRI as inhaled contrast agents for investigating lung structure and functioning. One of the directions in these investigations relies on studying ³He gas diffusion in lungs. As diffusion in lungs, especially, at the acinar level, is strongly restricted by alveoli, it might provide important insights on lung microstructure. To make this information quantitative, relationships between lung microstructure parameters and a diffusion attenuated MR signal are required. One of the

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approaches—*in vivo* lung morphometry technique [1]—is based on a well known geometrical model of the lung, in which acinar lung airways are considered as cylinders covered by alveolar sleeves [2]. Accordingly, in [1] diffusion of ³He gas in each airway is considered to be anisotropic and described by distinct longitudinal and transverse diffusion coefficients, D_L and D_T . Then, in each airway a MR signal with respect to *b*-value was assumed as:

$$S(b; \alpha) = S_0 \cdot \exp[-b \cdot D(\alpha)],$$

$$D(\alpha) = D_L \cos^2 \alpha + D_T \sin^2 \alpha,$$
(1)

where S_0 is the MR signal intensity in the absence of diffusion-sensitizing gradients, α is the angle between the diffusion gradient and the cylinder's axis, and the *b*-value is determined by the gradient waveform shape, strength,

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and timing. With the spatial resolution of several millimeters currently available with ³He MRI, each voxel contains hundreds of acinar airways with different orientations. Under a reasonable assumption of a uniform distribution of airway orientations, the total MR signal from a voxel is [1]:

$$S(b) = S_0 \exp(-bD_{\rm T}) \left(\frac{\pi}{4bD_{\rm AN}}\right)^{1/2} \cdot \Phi[(bD_{\rm AN})^{1/2}],$$
(2)

where $\Phi(x)$ is the error function and $D_{AN} = D_L - D_T$ is the diffusion anisotropy. This macroscopically isotropic but microscopically anisotropic model allows the estimation of these diffusion coefficients from multi-*b*-value MR measurements [1].

While some computer simulations of ³He gas diffusion in alveolar ducts [3,4] demonstrated a rather good agreement with the results of the model [1], no systematic study of the relationship between airway geometrical parameters and model parameters $(D_L \text{ and } D_T)$ has been conducted. This is a major subject of the current paper. Also in this paper we expand the theoretical model [1] by incorporating the effects of non-Gaussian signal behavior (i.e. the dependence of $D_{\rm L}$ and $D_{\rm T}$ on *b*-value). We focus our attention on diffusion at times Δ of several milliseconds, which is a typical diffusion time used in most experiments (see, e.g., [1,4-28]). Here a diffusing ³He atom samples a distance smaller than the acinar airway length but comparable with the airway radius. From a theoretical perspective, this diffusion time belongs to an intermediate regime where developing an analytical theory faces substantial difficulties. Thus, the problem is studied herein by means of computer Monte Carlo simulations.

Simulations uncovered remarkable scaling relationships between diffusion coefficients and lung geometrical parameters. This allowed presenting results in a rather compact form:

$$D_{\mathrm{L}} = D_{\mathrm{L}0} \cdot (1 - \beta_{\mathrm{L}} \cdot bD_{\mathrm{L}0}),$$

$$D_{\mathrm{T}} = D_{\mathrm{T}0} \cdot (1 + \beta_{\mathrm{T}} \cdot bD_{\mathrm{T}0}),$$
(3)

where

$$\begin{split} \frac{D_{\rm L0}}{D_0} &= 1 - \left(\frac{R}{L}\right)^{1/2} \cdot \left[1 - \exp\left(-2.5 \cdot \left(1 - \frac{r}{R}\right)^{1.8}\right)\right],\\ \beta_{\rm L} &= 43.5 \cdot \left(\frac{R}{L_{\rm diff}^{(1)}}\right)^2 \cdot \exp\left[-4 \cdot \left(1 - \frac{r}{R}\right)^{-1/2}\right],\\ \frac{D_{\rm T0}}{D_0} &= 0.44 \cdot \left(\frac{R}{L_{\rm diff}^{(2)}}\right)^{4 \cdot \left[1 - \left(R/L_{\rm diff}^{(2)}\right)^{0.7}\right]},\\ \beta_{\rm T} &= 0.09 \cdot \left(\frac{R}{L_{\rm diff}^{(2)}}\right)^{0.1 \cdot \left(L_{\rm diff}^{(2)}/R\right)^{3/2}}. \end{split}$$
(4)

Here D_0 is the free diffusion coefficient of ³He gas in lung airspaces; $L_{\text{diff}}^{(1)} = (2D_0\Delta)^{1/2}$ and $L_{\text{diff}}^{(2)} = (4D_0\Delta)^{1/2}$ are the characteristic free-diffusion lengths for one- and two-dimensional diffusion, respectively; *R* and *r* are the external



Fig. 1. Schematic structure of two levels of acinar airways. Open spheres represent alveoli forming an alveolar sleeve around each airway. Inset schematically represents the structure of the same airways in emphysema, scaled down for clarity.

and internal airway radii, *L* is the alveolar size, as defined in Fig. 1. With an average accuracy of about 1–3%, Eqs. (3) and (4) are valid within the intervals $R/L_{diff}^{(1)} < 0.7$ and r/R > 0.4. For typical diffusion time $\Delta = 1.8$ ms, $L_{diff}^{(1)}$ is 563 µm, so that *R* must be less than 400 µm. This interval covers not only typical radii of acinar alveolar ducts in healthy human lungs but those in small animals (e.g., mice, rats) as well.

Applying Eqs. (2)–(4) to multi-*b* measurements of the ³He diffusion attenuated MRI signal in lung airways makes possible the *in vivo* evaluation of mean geometrical parameters of lung acinar airways, in spite of the airways being too small to be resolved by direct imaging. MRI-based measurement of airways parameters in healthy and emphysematous lungs may provide an important non-invasive tool for identifying changes in lung structure at the alveolar level.

2. Methods

2.1. Geometrical model

According to the lung geometrical model [2] adopted in [1], acinar airways are considered as cylinders covered by sleeves formed by alveoli (open spheres in Fig. 1). The diagram defines inner (r) and outer (R) radii (as in Fig. 1 in [2]) and the distance between alveolar walls, L (this parameter can also be considered as a mean alveoli size). In humans, depending on the branching level of the acinar airway tree, the internal acinar airway radius r varies in the interval from 135 µm to 250 µm, whereas the outer radius R (including the sleeve of alveoli) remains practically constant at 350 µm [2]. Ninety-three percent of the gas is in

the acinar units, so restricting our simulations to acinar airways is a good approximation.

In the computer simulations below, we mimic an acinar airway by a periodic structure of cylindrical symmetry; one segment of the structure is shown in Fig. 2 (one of four alveoli is removed). The alveolar walls are considered impermeable to the gas atoms. A similar model of the alveolar duct was used for numerical solution of the diffusion equation in [29]; however, in our model as well as in the model used in [3], each alveolus covers 1/4 of an annular ring rather than 1/8 in [29]; we will demonstrate below that in the physiological range of r/R this difference is not important for diffusion calculations.

Our model of acinar airway is described by three geometrical parameters-external radius, R, internal radius, r, and the distance between alveolar walls, L. The intervals over which these parameters vary were chosen in the physiological range characteristic for healthy or slightly emphysematous human lungs or lungs of large animals. However, the scaling relationships that we found allow the application of the derived expressions to small animals as well. For Monte Carlo simulations we vary R in the interval 300-400 µm. The distance L, according to preliminary estimates, does not deviate from R more than 20%, therefore the simulations are performed in the range 0.8 < L/R < 1.2. Although the simulations were performed in the whole range of possible r (0 < r < R), attention is paid primarily to the physiological range r/R > 0.4.

2.2. Computer simulations

Computer simulations of random-walks were performed on *M* independent particles with random starting positions, with *M* typically 10^{6} – 10^{7} . At each computer step of duration Δt , a particle moves with equal probability in one of 8 directions (± 1 , ± 1 , ± 1) over distance $l_0 = (6D_0 \cdot \Delta t)^{1/2}$, where $D_0 = 0.88$ cm²/s is the free diffusion coefficient of ³He gas in N₂ or air. The time step was chosen to ensure that the distance l_0 is much smaller than any sizes of the geometrical model.

At each step j of a random walk through a magnetic field gradient, a particle gains a phase



Fig. 2. Model of acinar airway covered by alveolar sleeve (alveolar duct) corresponding to the structure depicted in Fig. 1. One segment of the periodic structure is shown; one of four alveoli is removed.

$$\Delta \psi_j = \gamma \mathbf{G}(t_j) \cdot \mathbf{r}(t_j) \cdot \Delta t, \tag{5}$$

where γ is the gyromagnetic ratio, $\mathbf{r}(t_j)$ is he position of the particle at step *j*, and $\mathbf{G}(t_j)$ is the time-dependent magnetic field gradient introduced as usual for diffusion encoding. The index *j* enumerates computer time steps running from 0 to $N = T/\Delta t$, where *T* is the full sequence time and $t_j = j \cdot \Delta t$. If a contemplated jump would pass through any boundary (see Fig. 2), the move was rejected and the particle remained at the initial position. For our simulations, we use $\Delta t = 1 \, \mu$ s, corresponding to the jump distance $l_0 = 23 \, \mu$ m. We have verified that using simulations with random step directions (rather than eight), and/or more complicated reflection laws, and/or shorter Δt does not affect the result of simulations; however, the use of these methods leads to longer computational times and were therefore not used.

The MR signal, *S*, was calculated by averaging signals from *M* individual particles:

$$S = \langle \exp(\mathrm{i}\psi) \rangle_M = \langle \cos\psi \rangle_M, \quad \psi = \sum_{j=0}^N \Delta\psi_j.$$
 (6)

The Monte Carlo algorithm was thoroughly tested to ensure its proper functioning by comparing the MR signal obtained by simulations with the exact analytical (or close-to-analytical) results known for simple geometries (one-dimensional interval, circle and sphere) [30,31]. The results of these simulations demonstrate excellent agreement with analytical predictions.

In most simulations, we use a diffusion sensitizing gradient waveform (see Fig. 3) with parameters similar to those in [1] and typical for human imaging: diffusion time $\Delta = \delta = 1.8$ ms, gradient ramp time $\tau = 0.3$ ms. However, as it will be demonstrated below, the results are valid for a rather broad range of diffusion parameters Δ , δ , and τ . The *b*-value corresponding to such a pulse sequence is equal to [1,32]:



Fig. 3. Diffusion sensitizing pulse gradient waveform employed in simulations.

$$b = (\gamma G_{\rm m})^2 \left[\delta^2 \left(\Delta - \frac{\delta}{3} \right) + \tau \left(\delta^2 - 2\Delta\delta + \Delta\tau - \frac{7}{6}\delta\tau + \frac{8}{15}\tau^2 \right) \right], \tag{7}$$

where $G_{\rm m}$ is the gradient amplitude. The simulations were performed for different orientations of the gradient with respect to the cylinder's axis and different gradient amplitudes $G_{\rm m}$; the *b*-dependent apparent diffusion coefficient $D(\alpha, b)$ was calculated as:

$$D(\alpha, b) = -\frac{1}{b} \ln S(\alpha, b).$$
(8)

In particular, if the gradient **G** is parallel to the cylinder's axis, $D(0, b) = D_L$; for **G** oriented perpendicular to the cylinder axis, $D(\pi/2, b) = D_T$. In what follows, the sequence timing parameters are kept constant and the *b*-value is altered from 0 to 10 s/cm² by changing the gradient amplitude G_m .

3. Results

3.1. Longitudinal diffusivity

To analyze the longitudinal diffusivity D_L , the simulations were performed with the gradient $\mathbf{G}(t)$ parallel to the cylinder axis. Obviously, in the case of smooth cylinders, diffusion in this direction would be free, and $D_L = D_0$. The internal boundaries depicted in Fig. 2 impede longitudinal diffusion, with a smaller internal radius *r* resulting in more restricted diffusion and a smaller longitudinal diffusivity D_L .

Fig. 4 illustrates the dependence of $D_{\rm L}$ on the *b*-value for different internal radii *r*. In the simulations shown below, we use $R = L = 350 \,\mu\text{m}$ which corresponds to a typical



Fig. 4. The longitudinal diffusivity $D_{\rm L}$ as a function of the *b*-value for different internal radii *r* (shown by numbers near the lines; in µm). Symbols represent the results of simulations; straight lines—linear fit to Eq. (9). $R = L = 350 \ \mu\text{m}$, $\Delta = 1.8 \ \text{ms}$, $\tau = 0.3 \ \text{ms}$. Data are truncated for $bD_{\rm L} > 2$, corresponding to the MR signal decay of e^{-2} .

alveolar duct size in healthy lungs. In the case r = R corresponding to free diffusion in the direction parallel to the cylinder's axis, $D_{\rm L} = D_0$ and does not depend on the *b*-value, as expected. For all other values of r < R, diffusion is restricted and $D_{\rm L}$ depends on *b*. In the most interesting physiological range of r (150–200 µm), the slope reaches its maximum; for instance, for r = 150 µm the longitudinal diffusivity $D_{\rm L}$ changes from 0.35 cm²/s at b = 0.5 s/cm² to 0.25 cm²/s at b = 10 s/cm² (30% decrease).

This *b*-dependence of $D_{\rm L}$ can be well approximated by a linear function,

$$D_{\rm L} = D_{\rm L0} \cdot (1 - \beta_{\rm L} \cdot b D_{\rm L0}). \tag{9}$$

The coefficients D_{L0} and β_L being found by fitting Eq. (9) to the data for $D_{\rm L}(b)$ by means of a standard Levenberg-Markquart algorithm. The same algorithm was used for fitting procedures all over the study. The sign "-" in Eq. (9) is chosen for convenience because the slope of the functions $D_{\rm L}(b)$ is positive only for the line corresponding r=0(completely closed cylinder) and negative for all the other lines shown in Fig. 4. Note that the coefficient $\beta_{\rm L}$ (and a similar coefficient β_{T} in the transverse diffusivity, see Eq. (16) below) reflects non-Gaussian diffusion effects in each individual airway and is proportional to the so called kurtosis K-the second order term in the cumulant expansion of the MR signal (e.g., [33–35]); $(K_{\rm L} = 6\beta_{\rm I}, K_{\rm T} = -6\beta_{\rm T})$. It should be emphasized, however, that the original model for the signal S(b) in Eq. (2) also demonstrated non-monoexponentiality in b-value, which was due to orientation averaging of the signals from individual airways $S(b; \alpha)$, Eq. (1). The non-monoexponentiality in b-value described by coefficients $\beta_{\rm L}$ and $\beta_{\rm T}$ for individual orientations and thus is in addition to this "averaging" effect.

To analyze the dependence of the phenomenological parameters D_{L0} and β_{L} on airway geometrical characteristics, we note that the system under consideration is characterized by four parameters of length: R, L, r, and the $L_{\rm diff}^{(1)} = (2D_0\Delta)^{1/2}$ diffusion characteristic distance $(L_{\text{diff}}^{(1)} = 563 \,\mu\text{m} \text{ for } \Delta = 1.8 \,\text{ms} \text{ used in our simulation}).$ Therefore, the parameters D_{L0} and β_L in Eq. (9) may depend, generally, on three-dimensionless ratios: r/R, L/R and $R/L_{diff}^{(1)}$. Fig. 5 illustrates the dependences of $D_{\rm L0}$ and $\beta_{\rm L}$ on the dimensionless parameter r/R for R =350 μ m and different L (300, 350, and 400 μ m). The parameter D_{L0} monotonically increases from small values at r = 0and tends to the free diffusion coefficient $D_0 = 0.88 \text{ cm}^2/\text{s}$ at $r/R \rightarrow 1$. The parameter β_1 rapidly increases from small negative values at r = 0, reaching its maxima at $r/R \sim 0.2$ and then monotonically decreasing to 0 at $r/R \rightarrow 1$. Such behavior of the parameter $\beta_{\rm L}$ should be expected because at r = 0 the airway is completely closed and longitudinal diffusion is strongly restricted by the alveolar walls separated by the distance L, which is smaller than the diffusion distance $L_{\text{diff}}^{(1)}$. In this limit, diffusion can be approximately described by the Gaussian phase approximation, where the signal is close to monoexponential with respect to *b*-value (for fixed Δ). In the opposite limit $r/R \rightarrow 1$



Fig. 5. The parameters D_{L0} (a) and β_L (b) as functions of r/R for $R = 350 \ \mu\text{m}$ and different L.

diffusion becomes free and once again the signal behavior is monoexponential with b. In both these case $\beta_{\rm L}$ tends to zero, as in Fig. 5b.

Simulations with different external radii *R* and distances L ($R = 300 \ \mu\text{m}$ and $L = 250-350 \ \mu\text{m}$; $R = 350 \ \mu\text{m}$ and $L = 300-400 \ \mu\text{m}$; $R = 400 \ \mu\text{m}$ and $L = 350-450 \ \mu\text{m}$) reveal a remarkable scaling relationship that is valid in the physiologically important range of parameters, r/R > 0.4:

$$\frac{D_{\rm L0}}{D_0} = 1 + \left(\frac{R}{L}\right)^{1/2} \cdot f\left(\frac{r}{R}\right),\tag{10}$$

This result is demonstrated in Fig. 6, where the quantity $(D_{L0}/D_0 - 1) \cdot (L/R)^{1/2}$ is plotted as a function of r/R for all the sets of R and L mentioned above. All the lines (shown by symbols in Fig. 6) corresponding to different R and L have collapsed to one universal curve, f(r/R). This means that the parameter D_{L0} depends on the external radius R only through the ratios L/R and r/R, Eq. (10), and does not depend on the third dimensionless ratio $R/L_{diff}^{(1)}$.



Fig. 6. The quantity $(D_{L0}/D_0 - 1) \cdot (L/R)^{1/2}$ as a function of r/R for different R and L (symbols). Solid line—the function f(r/R), Eq. (11).

We found that the function f(r/R) can be well approximated by the following analytical expression, shown as the solid line in Fig. 6:

$$f(r/R) = \exp[-2.5 \cdot (1 - r/R)^{1.8}] - 1.$$
(11)

Apparently, there exist many other analytical expressions that can be used for describing the function f(r/R) with the same accuracy. In our study we tried to choose an expression that would require a minimal number of fitting parameters (e.g., two numerical coefficients in Eq. (11)). For example, an attempt to approximate the function f(r/R) with the same accuracy by a polynomial expression would require, at least, four numerical coefficients. The same principle for selecting the structure of analytical expressions used for fitting Monte Carlo generated diffusion data was exercised throughout the study. Combining Eqs. (10) and (11), D_{L0} can be related to the geometrical parameters of the model as follows:

$$\frac{D_{L0}}{D_0} = 1 - \left(\frac{R}{L}\right)^{1/2} \cdot \left[1 - \exp\left(-2.5 \cdot \left(1 - \frac{r}{R}\right)^{1.8}\right)\right].$$
(12)

Consider parameter $\beta_{\rm L}$. As seen from Fig. 5b, in the range r/R > 0.4 the parameter $\beta_{\rm L}$ is practically independent of *L*. In contrast to $D_{\rm L0}$, however, $\beta_{\rm L}$ depends on the external radius *R* not only through the ratio r/R but on the ratio $R/L_{\rm diff}^{(1)}$ as well (see Fig. 7a). An analysis shows that in the range r/R > 0.4, $\beta_{\rm L}$ scales as $\left(R/L_{\rm diff}^{(1)}\right)^2$:

$$\beta_{\rm L} = \left(\frac{R}{L_{\rm diff}^{(1)}}\right)^2 \cdot g\left(\frac{r}{R}\right). \tag{13}$$

This is demonstrated in Fig. 7b, where the quantity $\beta_{\rm L} \cdot \left(L_{\rm diff}^{(1)}/R\right)^2$ is plotted as a function of r/R for different R; the lines corresponding to different R have collapsed in one universal curve. The function g(r/R) can be well



Fig. 7. The parameter $\beta_{\rm L}$ (a) and $\beta_{\rm L} (L_{\rm diff}^{(1)}/R)^2$ as functions of r/R for different external radii R. Solid line in (b)—the function g(r) in Eq. (14).

approximated by the following expression, shown as the solid line in Fig. 7b:

$$g(r/R) = 43.5 \cdot \exp[-4(1-r/R)^{-1/2}].$$
 (14)

Combining Eqs. (13) and (14), the parameter β_L can be related to the geometrical parameters of the model as follows:

$$\beta_{\rm L} = 43.5 \cdot \left(\frac{R}{L_{\rm diff}^{(1)}}\right)^2 \cdot \exp\left[-4\left(1-\frac{r}{R}\right)^{-1/2}\right].$$
 (15)

3.2. Transverse diffusivity

To analyze the transverse diffusivity $D_{\rm T} = ADC(\alpha = \pi/2)$, the simulations were performed with the gradient **G**(*t*) perpendicular to the cylinder axis. Transverse diffusion is restricted by the external boundary (airway wall, a cylinder of radius *R*) and by the internal boundaries (alveolar sleeve) (see Fig. 2). As the internal boundaries violate the cylindrical symmetry of the system, the MR signal attenuation and $D_{\rm T}$ may, in the general case,

depend upon the orientation of the magnetic field gradient **G** within the cylinder's cross-sectional plane with respect to the internal boundaries. Our simulations showed that for the sequence parameters used and typical radii of the airways, this dependence is rather weak: the maximum difference in $D_{\rm T}$ found for different orientations increases with *b*-value but does not exceed 5% at $b = 10 \text{ s/cm}^2$. In what follows, we average the signal over these orientations and present average values of the transverse diffusivity $D_{\rm T}$.

Fig. 8 illustrates the transverse diffusivity $D_{\rm T}$ as a function of *b*-value for different internal radii *r*. As in the case of longitudinal diffusion, $D_{\rm T}$ reveals a linear dependence on the *b*-value similar to Eq. (9),

$$D_{\mathrm{T}} = D_{\mathrm{T0}} \cdot (1 + \beta_{\mathrm{T}} \cdot b D_{\mathrm{T0}}). \tag{16}$$

However, in contrast to Fig. 4 for $D_{\rm L}$, the slope in $D_{\rm T}$ in Fig. 8 is negative for the line corresponding r = 0 and positive otherwise. For the selected diffusion gradient waveform and typical parameters of lung airways, the dependence of the transverse diffusion coefficient $D_{\rm T}$ on the *b*-value is substantially smaller than in the case of $D_{\rm L}$. For instance, for $r = 150 \,\mu\text{m}$, $D_{\rm T}$ changes from 0.090 cm²/s at $b = 0.5 \,\text{s/cm}^2$ to 0.095 cm²/s at $b = 10 \,\text{s/cm}^2$ (a 5% increase).

The dependence of the parameters D_{T0} and β_T in Eq. (16) on the ratio r/R for different external radii R is demonstrated in Fig. 9. The parameters D_{T0} and β_T rapidly increase as the internal radius increases. However, in the physiological range r/R > 0.4, D_{T0} and β_T depend on the ratio r/R rather weakly and, therefore, can be approximated by their values at r = R. For small radii, where $R \ll L_{diff}^{(2)}$ and diffusion falls in the motion narrowing regime, diffusion can be described in the framework of the well known Gaussian phase approximation [31,36], in which the MR signal is mono-exponential in *b*-value ($\beta_T = 0$) and



Fig. 8. The transverse diffusivity $D_{\rm T}$ as a function of the *b*-value for different internal radii *r* (shown by numbers near the lines; in µm). Symbols represent the results of simulations; straight lines—linear fit to Eq. (16). $R = 350 \,\mu\text{m}$, parameters of gradient waveform the same as in Fig. 4.

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Fig. 9. The dependence of the parameters D_{T0} and β_T in the linear fit (16) on the ratio r/R for different external radii R.

$$\frac{D_{\rm T0}}{D_0} \sim \left(\frac{R}{L_{\rm diff}^{(2)}}\right)^4,\tag{17}$$

where $L_{\text{diff}}^{(2)} = (4D_0\Delta)^{1/2}$ is the characteristic distance for twodimensional diffusion (obviously, diffusion in the transverse plane is better characterized by the two-dimensional characteristic distance $L_{\text{diff}}^{(2)}$ rather than the one-dimensional distance $L_{\text{diff}}^{(1)}$ used above for longitudinal diffusion; $L_{\text{diff}}^{(2)} = L_{\text{diff}}^{(1)} \cdot \sqrt{2} = 796 \,\mu\text{m}$ for $\Delta = 1.8 \,\text{ms}$ used in our simulation). Our analysis shows that for the external radii 200 $\mu\text{m} < R < 500 \,\mu\text{m}$, the parameter $D_{\text{T0}} \approx D_{\text{T0}}(r = R)$ can be well approximated by the following modification of Eq. (17):

$$\frac{D_{\rm T0}}{D_0} = 0.44 \cdot \left(\frac{R}{L_{\rm diff}^{(2)}}\right)^{4 \cdot \left[1 - \left(R/L_{\rm diff}^{(2)}\right)^{0.7}\right]}.$$
(18)

The parameter $\beta_{\rm T} \approx \beta_{\rm T}(r=R)$ in the range of *R* (300 μ m $< R < 400 \,\mu$ m) can be approximated as

$$B_{\rm T} = 0.09 \cdot \left(\frac{R}{L_{\rm diff}^{(2)}}\right)^{0.1 \cdot \left(L_{\rm diff}^{(2)}/R\right)^{3/2}}.$$
(19)

4. Assumptions and restrictions

The empirical equations (4) are obtained by using simulations with specific timing of the pulse sequence and within certain intervals of the geometrical parameters: $\Delta = \delta = 1.8$ ms, $R = 300-400 \mu m$. This diffusion time corresponds to the characteristic one- and two-dimensional diffusion lengths $L_{diff}^{(1)} = 563 \mu m$ and $L_{diff}^{(2)} = L_{diff}^{(1)} \sqrt{2} = 796 \mu m$. It is important to note that Δ appears in Eq. (4) only via the dimensionless ratios $R/L_{diff}^{(1,2)} \sim R/\Delta^{1/2}$. As R varies in our simulations between 300 and 400 µm, the parameter $R/L_{diff}^{(1)}$ changes in the interval $0.5 < R/L_{diff}^{(1)} < 0.7$. It means that Eq. (4) are valid for arbitrary R and Δ , provided that the ratio $R/L_{diff}^{(1)}$ remains within this interval. Since all the expressions in Eq. (4) depend only on the ratios of the parameters, this suggests that the actual applicability of these equations may be broader than specified above.

Consider first the longitudinal diffusivity D_{L0} that was calculated for $L_{diff}^{(1)} = 563 \,\mu\text{m}$ and airway radii R in the range of 300–400 μm $\left(L_{diff}^{(1)} > R \text{ and } L\right)$. Because the expression for D_{L0} , Eq. (12), does not depend on diffusion time Δ and the parameter β_L decreases as Δ decreasing, we can expect that the system approaches the limit of 1D "quasi-free" diffusion in which the diffusion propagator tends to a Gaussian. In this case, Eq. (12) for D_{L0} and Eq. (15) for β_L are not restricted by $0.5 < R/L_{diff}^{(1)} < 0.7$ but are expected to remain valid for all $R/L_{diff}^{(1)} < 0.7$. To test this supposition, we simulated data with R = 100 and 200 μ m. Confirming our hypothesis, we found that for these radii, the dependences of $(D_{L0}/D_0 - 1) \cdot (L/R)^{1/2}$ and $\beta_L \cdot (L_{diff}^{(1)}/R)^2$ on the ratio r/R fall on the same universal curves for all combinations of R and L, as shown in Figs. 6b and 7.

To find the range of parameters where Eqs. (18) and (19) for transverse diffusivity are valid, we generated Monte Carlo data for R in the interval from 100 µm to 1500 µm. The results for D_{T0} and β_T as functions of $R/L_{diff}^{(2)}$ are shown in Fig. 10 along with the values obtained using Eqs. (18) and (19). One can see that for $R/L_{diff}^{(2)} < 0.75$ (corresponding to R < 600 µm for $L_{diff}^{(2)} = 796$ µm), the empirical Eqs. (18) and (19) describe D_{T0} very well. The interval R < 600 µm is in the range of lung parameters for healthy humans and smaller animals, as well as for human lungs with mild emphysema. For $R/L_{diff}^{(2)} > 0.75$, the approximation (18) becomes meaningless because it predicts the decrease in D_{T0} rather than its increase up to D_0 in the free diffusion limit $R \gg L_{diff}^{(2)}$ (see Fig. 10a). In this interval, another approximation for D_{T0} can be used (shown by dashed line in Fig. 10a):



Fig. 10. The dependence of the parameters $D_{\rm T0}$ and $\beta_{\rm T}$ on the external radius *R* (symbols). Solid lines—approximation by Eqs. (18) and (19); dashed line—approximation by Eq. (20). The function $\beta_{\rm T}(R/L_{\rm diff}^{(2)})$ is shown only for $R/L_{\rm diff}^{(2)} < 0.6$, where the linear approximation, Eq. (16), is valid.

$$D_{\rm T0} = D_0 \cdot \exp\left[-0.73 \cdot \left(L_{\rm diff}^{(2)}/R\right)^{1.4}\right].$$
 (20)

Note that for small $R/L_{\rm diff}^{(2)}$ the approximation Eq. (20) is less accurate than the approximation given by Eq. (18). Also note that for $R > 500 \,\mu m \, (R/L_{\rm diff}^{(2)} > 0.6)$ the dependence of the transverse diffusivity $D_{\rm T}$ on *b*-value cannot be described by a linear approximation (16) but requires at least a quadratic term proportional to b^2 .

Thus, we can state that the empirical expressions describing the longitudinal and transverse diffusivity as functions of geometrical parameters, Eq. (4), appear to be valid for $R/L_{diff}^{(1)} \leq 0.7$. For $L_{diff}^{(1)} = 563 \,\mu\text{m}$ this corresponds to $R \leq 400 \,\mu\text{m}$, which covers not only the typical radii of acinar alveolar ducts in healthy human lungs but those in small animals (mice, rats) as well. Note also that this interval can be changed by changing the diffusion time: for longer Δ (and, correspondingly, longer $L_{diff}^{(1)}$) the model

can be applied for bigger radii R; for shorter Δ , the interval shifts towards smaller values of R. The interval can be also changed if the free diffusion coefficient D_0 is different from that used in our study, making it possible to apply the model, for instance, to ¹²⁹Xe for which D_0 is substantially smaller than in ³He.

In our simulations, we considered the acinar airways as infinitely long, ignoring their branching. This simplification is valid when a mean displacement of ³He atoms along the airway's principal axis during diffusion sensitizing gradients, $(2D_L\Delta)^{1/2}$, is smaller than the mean length of alveolar ducts and sacs. In human lungs, this mean length is about 1 mm [2]. For a typical longitudinal diffusivity $D_L \sim 0.4 \text{ cm}^2/\text{s}$, this condition imposes a restriction on diffusion time: $\Delta < 10 \text{ ms}$. For longer diffusion times, a more general theory accounting for branching of acinar airways is required.

It should also be noted that Eq. (4) do not contain another time parameter—the ramp time τ ($\tau = 0.3$ ms in our simulations). Obviously, this parameter is expected not to affect the structure of Eq. (4) if $\tau \ll \Delta$. Our simulations demonstrate that for τ varying in the range $0 < \tau < 0.6$ ms, an error in determination of *R* and *r* from fitting of Eqs. (3) and (4) to the simulated data does not exceed 5–6% when the *b*-value is calculated according to Eq. (7). Only for a maximally long triangular gradient pulse, $\tau = \Delta/2 = 0.9$ ms, does the error reach 15%.

It is interesting also to note that for $R/L_{\text{diff}}^{(1)} \leq 0.7$, the parameter D_{L0} does not depend on the structure of pulse gradient at all; even for narrow pulses, when $\delta \ll \Delta$, its dependence on r/R falls on the same universal curve given by Eq. (12). However, it is not the case for D_{T0} , which is strongly affected by the structure of the gradient pulse; for instance, in the limit $R/L_{\text{diff}}^{(2)} \ll 1 D_{\text{T0}}$ depends on R as R^4 in the case of spin echo gradient pulses ($\delta = \Delta$), whereas for very narrow pulses, when $\delta \ll \Delta$, $D_{\text{T0}} \sim R^2$.

In the geometrical model of acinar airways, we assumed that each alveolus covers 1/4 of the annular ring. Obviously, the number of alveoli (in our case, 4) in the ring may affect the transverse diffusivity $D_{\rm T}$ because each wall between alveoli imposes an additional obstacle for diffusing atoms. However, as demonstrated in the previous section, in the physiological range r/R > 0.4, the transverse diffusivity $D_{\rm T}$ is practically independent of the internal radius r and, consequently, of the number of alveoli per the annual ring.

Eqs. (2)–(4) are quantitatively valid in the physiologically important range of the airways parameters characteristic of healthy lungs and lungs with mild emphysema, cases in which acinar airways can be modeled as cylinders covered with an alveolar sleeve. With emphysema progression, the "cylindrical" model is expected to fail, as airway and alveolar walls can develop holes and become permeable to diffusing ³He atoms. In lungs with advanced emphysema, our results might provide only the "apparent" characteristics (R, r, L) but these still can potentially be used to evaluate emphysema progression. A detailed analysis of the role of wall permeability on the behavior of the diffusion attenuated MR signal was previously developed for a simple model [37]. For lungs with substantial degeneration of the acinar walls, our model should also be generalized to account for the development of large air cavities in which ³He atom diffusion is much less restricted. All these effects are beyond the scope of the current paper and will be the subject of future studies.

A detailed analysis of the accuracy in estimating parameters $D_{\rm L}$ and $D_{\rm T}$ for the model in Eq. (2) was published previously [38]. It was demonstrated there that a rather high SNR (on the order of 100) is required for the evaluation of these parameters. Here we only briefly expand on this subject by evaluating errors in estimating geometrical parameters of our model for typical lung physiological parameters. To estimate the influence of noise on the accuracy of the fitting procedure, Gaussian noise was added to the "ideal" signal S(b) calculated by means of Eqs. (2)–(4) with known R, r, L. This data set was then analyzed according to Eqs. (2)-(4) to obtain the estimated values of the geometrical parameters, R_e , r_eL_e . This procedure was repeated numerous times and the estimated values were statistically analyzed. For $R = L = 350 \,\mu\text{m}, r =$ 180 μ m and SNR = 100, we obtained $R_e = 360 \pm 27 \mu$ m, $r_{\rm e} = 176 \pm 13 \ \mu {\rm m}, \ L_{\rm e} = 351 \pm 66 \ \mu {\rm m}.$ Note that the standard deviation in L_e is a substantially higher fraction than for the two other parameters. This can be explained by the specific structure of Eq. (4), where the parameter L appears only in the equation for D_{L0} , and the dependence of the latter on L is rather weak. Moreover, when the internal radius r is close to the external radius R, D_{L0} becomes practically independent of L (see Fig. 5) and the accuracy in determination of parameter L becomes even worse.

5. Discussion

The model of diffusion attenuated MRI signal in lung proposed in [1] contains three parameters: the signal amplitude S_0 , and the longitudinal and transverse diffusivities in a single airway— D_L and D_T . Eq. (1) for an individual airway implies that the signal is mono-exponential in *b*-value, $D_{\rm L}$ and $D_{\rm T}$ being independent of b. Our simulations, however, reveal that for the pulse sequence parameters used in [1] ($\Delta = 1.8 \text{ ms}, b = 0-10 \text{ s/cm}^2$), both diffusivities demonstrate a linear dependence on the b-value—Eqs. (9) and (16). This effect is stronger for the longitudinal diffusivity, resulting on average in a 10% decrease in $D_{\rm L}$ (but up to 30% for some parameter combinations) as b increases to about 10 s/cm². The transverse diffusivity $D_{\rm T}$ also increases with b value; however, the effect is smaller—about 5%. To incorporate these dependences in our model, the expression (2) for the signal as a function of the b-value is modified according to Eq. (3). The relationships between the parameters entering Eq. (3) and the geometrical parameters of airways—R, r, and L—are given in Eq. (4). Eq. (2) for the signal along with Eqs. (3) and (4) for the longitudinal and transverse diffusivities make it possible to determine

all three geometrical parameters of the airways: R, r, and L from multi-b measurements.

As an example, we have re-analyzed previously published data obtained with ³He diffusion MRI in a dog model of unilateral emphysema [26]. The theoretical model Eqs. (2)–(4) with four adjustable parameters (S_0 , R, r, L) provides a very good fit to experimental data, as in Fig. 11. As expected, in compressed lungs, contralateral to the hyper-inflated emphysematous lungs, the external and internal radii of acinar airways are smaller than in the normal healthy lungs, whereas in lungs with mild emphysema they are larger.

In most experimental studies of gas diffusion in the lungs, only the mean isotropic ADC has been measured (e.g., [4-25,27,28]). Data obtained in these studies, even on healthy humans, exhibit rather broad variability—ADC as low as $0.15 \text{ cm}^2/\text{s}$ and as high $0.25 \text{ cm}^2/\text{s}$ were reported. This variability can be attributed to several causes: natural physiological inter-subject differences, ADC dependence on the strength of diffusion sensitizing gradients, and ADC dependence on the diffusion time. In most experimental studies, ADC is determined from measurements with small *b*-values because this ADC reflects underlying properties of the lung tissue and does not depend on the gradient strength is rather weak (e.g., [1,4,27]). In the limit of small *b*-values, ADC has a simple



Fig. 11. In vivo diffusion attenuated MR signal as a function of the *b*-value for the dog model. Symbols are data from Fig. 4 in [26]. Circles represent an example of the data from a normal lung. Squares and triangles represent an example of the data from a dog with experimentally induced unilateral emphysema. The emphysematous lung demonstrates enlarged airways and a corresponding increase in the signal decay. The contralateral lung appears compressed with smaller than normal airways, demonstrating slower than normal signal decay. Solid lines—fitting of Eqs. (2)– (4) to experimental data. Fitting resulted in the following evaluation of acinar airways geometrical parameters. In the compressed lungs: $R = 253 \pm 24 \,\mu\text{m}$, $r = 65 \pm 7 \,\mu\text{m}$, $L = 290 \pm 32 \,\mu\text{m}$; in the normal lungs: $R = 283 \pm 10 \,\mu\text{m}$, $r = 106 \pm 2 \,\mu\text{m}$, $L = 310 \pm 13 \,\mu\text{m}$; in the lungs with mild emphysema: $R = 355 \pm 5 \,\mu\text{m}$, $r = 278 \pm 3 \,\mu\text{m}$, $L = 290 \pm 49 \,\mu\text{m}$.

Table 1

A comparison of literature values for ³He ADC in healthy human lungs with that predicted by Eq. (21) assuming $R = L = 350 \,\mu\text{m}$, $r = 180 \,\mu\text{m}$

Reference	Diffusion time Δ (ms)	Reported mean ADC (cm ² /s)	ADC from Eq. (21) (cm ² /s)
Salerno et al. [9]	1.8-5.8	0.22-0.15	0.20-0.16
Saam et al. [7]	1.9	0.205	0.195
Morbach et al. [19]	2.3	0.17	0.18
Swift et al. [21]	1.46	0.21	0.215
Altes et al. [22]	1.6	0.24	0.21
Trampel et al. [23]	1.28	0.22	0.23

relationship to D_{L0} and D_{T0} introduced in our current model (see also [1]):

ADC =
$$\frac{1}{3}(D_{L0} + 2D_{T0}).$$
 (21)

Eq. (4) predict the dependence of ADC on the diffusion time Δ via the parameter D_{T0} . Although D_{T0} is smaller than D_{L0} , its contribution to variations in ADC is substantial. For example, for typical acinar airway parameters $R = L = 350 \,\mu\text{m}$, $r = 180 \,\mu\text{m}$, the ADC (21) changes from 0.26 cm²/s to 0.17 cm²/s when Δ changes from 1 ms to 3 ms. Unfortunately, in a majority of experimental reports diffusion time is not provided, we can therefore compare our results with only a few publications, see Table 1.

Thus, our theoretical predictions are in rather good agreement with experimental data. It should be noted, however, that Table 1 does not provide an explanation of experimental data, it just serves to demonstrate that some of the reported variations in ADC in healthy subjects may be due to variations in the diffusion time.

6. Conclusion

The ³He MR diffusion attenuated MR signal in normal lungs and lungs with mild emphysema is analyzed by means of computer Monte Carlo simulations. Empirical relationships between the longitudinal and transverse diffusivities in acinar airways and mean geometrical parameters of airways are found. These relationships are incorporated into the previously developed mathematical model of the signal [1] used for post-imaging analysis of experimental data obtained by multi-*b* measurements. This creates a basis for *in vivo* lung morphometry—the evaluation of acinar airway geometrical parameters from hyperpolarized ³He diffusion MRI.

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